CHAPTER 2

P2.1* (a) $R_{eq} = 25 \Omega$ (b) $R_{eq} = 25 \Omega$

P2.12 By symmetry, we find the currents in the resistors as shown below:



Then, the voltage between terminals a and b is $v_{ab} = R_{eq} = 1/3 + 1/6 + 1/3 = 5/6$

P2.24 In a similar fashion to the solution for Problem P2.6, we can write the following expression for the resistance seen by the 2-V source.

$$R_{eq} = 1 + \frac{1}{1/R_{eq} + 1/2}$$

The solutions to this equation are $R_{eq} = 2 \Omega$ and $R_{eq} = -1 \Omega$. However, we reason that the resistance must be positive and discard the negative root. Then, we have $i_1 = \frac{2V}{R_{eq}} = 1 A$, $i_2 = i_1 \frac{R_{eq}}{2 + R_{eq}} = \frac{i_1}{2} = 0.5 A$, and $i_3 = \frac{i_1}{2} = 0.5 A$. Similarly, $i_4 = \frac{i_3}{2} = \frac{i_1}{2^2} = 0.25 A$ and $i_{18} = \frac{i_1}{2^9} = 1.953 \text{ mA}$. P2.36^{*} Combining R_2 and R_3 , we have an equivalent resistance

$$R_{eq} = \frac{1}{1/R_2 + 1/R_3} = 10 \,\Omega.$$
 Then using the voltage-division principle, we have

$$v = \frac{R_{eq}}{R_1 + R_{eq}} \times v_s = \frac{10}{20 + 10} \times 10 = 3.333 \,V.$$

P2.39* Writing a KVL equation, we have $v_1 - v_2 = 10$. At the reference node, we write a KCL equation: $\frac{v_1}{5} + \frac{v_2}{10} = 1$. Solving, we find $v_1 = 6.667$ and $v_2 = -3.333$. Then, writing KCL at node 1, we have $i_s = \frac{v_2 - v_1}{5} - \frac{v_1}{5} = -3.333$ A.

P2.51 First, we can write: $i_{x} = 10i_{x} - v_{2}$

$$\dot{I}_x = \frac{10 I_x}{5}$$

Simplifying, we find $i_x = 0.2v_2$.

Then write KCL at nodes 1 and 2:

$$\frac{v_1 - 10i_x}{10} = -3 \qquad \frac{v_2}{20} - i_x = 1$$

Substituting for i_x and simplifying, we have

$$v_1 - 2v_2 = -30$$
 and $-.15v_2 = 1$
which yield $v_1 = -43.333$ V and $v_2 = -6.667$ V.

P2.61* Because of the current sources, two of the mesh currents are known.



Writing a KVL equation around the middle loop we have $20(i_1 - 1) + 10i_1 + 5(i_1 + 2) = 0$ Solving, we find $i_1 = 0.2857$.

P2.72 Open-circuit conditions:



$$i_x = \frac{20 - v_{oc}}{5}$$
 $\frac{v_{oc}}{10} - i_x + 0.5i_x = 0$ Solving, we find $v_{oc} = 10$ V

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Short-circuit conditions:

$$i_x = 20/5 = 4 \text{ A}$$

 $i_{sc} = i_x - 0.5 i_x = 2 \text{ A}$

Then we have

 $R_t = v_{oc} / i_{sc} = 5 \Omega$. Thus the equivalents are:



P2.75* To maximize the power to R_{L} , we must maximize the voltage across it. Thus we need to have $R_{t} = 0$. The maximum power is

$$P_{\max}=\frac{20^2}{5}=80\,\mathrm{W}$$

P2.85 (a) With only the 2-A source activated, we have $i_2 = 2$ and $v_2 = 2(i_2)^3 = 16$ V

(b) With only the 1-A source activated, we have $i_1 = 1 \text{ A}$ and $v_1 = 2(i_1)^3 = 2 \text{ V}$

(c) With both sources activated, we have

$$i = 3$$
 A and $v = 2(i)^3 = 54$ V

Superposition does not apply because device A has a nonlinear relationship between v and i.

P2.87* (a) Rearranging Equation 2.80, we have

$$\mathcal{R}_3 = \frac{\mathcal{R}_1}{\mathcal{R}_2} \mathcal{R}_x = \frac{10 \, k\Omega}{10 \, k\Omega} \times 5932 = 5932 \, \Omega$$

(b) The circuit is:



The Thevenin resistance is

$$R_{r} = \frac{1}{1/R_{3} + 1/R_{1}} + \frac{1}{1/R_{2} + 1/R_{x}} = 7447 \ \Omega$$

The Thevenin voltage is

$$V_{\tau} = V_{s} \frac{R_{3}}{R_{1} + R_{3}} - V_{s} \frac{R_{x}}{R_{x} + R_{2}}$$

 $= 0.3939 \, mV$

Thus, the equivalent circuit is:



Thus the detector must be sensitive to very small currents if the bridge is to be accurately balanced.